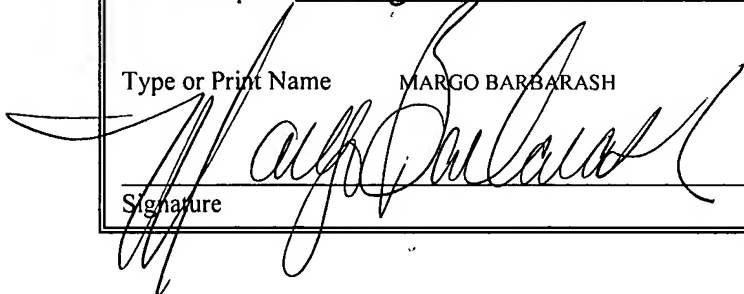


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**PROCESS FOR SAMPLING THE SIGNAL DELIVERED BY AN ACTIVE PIXEL OF  
AN IMAGE SENSOR, AND CORRESPONDING SENSOR**

**PRIORITY CLAIM**

[1] The present application claims priority from French Application for Patent No. 03 05363 filed April 30, 2003, the disclosure of which is hereby incorporated by reference.

**BACKGROUND OF THE INVENTION**

Technical Field of the Invention

[2] The present invention relates to processing of signals delivered by a matrix of pixels of an image sensor, and more particularly, to improving the performance in terms of dynamics and noise of the sampling of the signal emanating from a matrix of active pixels that is embodied in CMOS technology.

Description of Related Art

[3] An image sensor conventionally comprises a matrix of pixels. Each pixel delivers an electrical signal whose level depends on the quantity of light received by the pixel. This signal is conventionally stored in a pair of sampling capacitors and then it is, for example, amplified in a readout amplifier.

[4] Traditionally, the noise floor of a CMOS image sensor was limited by the pixel reinitialization noise, which is of the order of 1 millivolt rms. Solutions now exist for overcoming this noise. So, the limitation as regards noise is now shifted to the level of the samplers. More precisely, the passage of the bias current through the pixel follower transistor causes white noise, whose bandwidth is limited by the impedance of the transistor and the total capacitance of the sampling capacitor (for example, of the order of 0.5 pF) and of the column (bit line) (for example of the order of 1 pF). However, this current is dimensioned in respect of speed and accuracy constraints, and it is typically of the order of 1 microampere, thus making it possible to sample in approximately one microsecond.

[5] Moreover, the current source also participates in the white noise. At present, this white noise has a mean value estimated at approximately 150 microvolts.

[6] Additionally, the larger the gate-source voltage of the follower transistor, the more limited the usable signal range. Also, the gate-source voltage is related to the square root of the ratio of the current of the follower transistor to a coefficient dependent on the technological characteristics of the transistor. However, having regard to the dimensional constraints of the pixel, this technological coefficient can scarcely be increased in practice. Consequently, the current which passes through the follower transistor fixes the value of the

gate-source voltage  $V_{gs}$ . One is accordingly constrained to have a high gate-source voltage, the consequence being the clipping of the sampled signal.

[7] There is a need in the art to solve this problem. There is also a need to reduce the sampling noise. Still further, there is a need to reduce the gate-source voltage of the follower transistor in such a way as to utilize more useful signal without clipping.

#### SUMMARY OF THE INVENTION

[8] One embodiment of the invention proposes a process for sampling the signal delivered by an active pixel of an image sensor. The image sensor comprises a phase of storage of the signal in a pair of sampling capacitors comprising two successive respective effective electrical links of the two sampling capacitors with a follower transistor tracking the pixel in the course of the two respective sampling pulses corresponding respectively to two successive different levels of pixel voltage that are applied to a gate of the follower transistor.

[9] According to a general characteristic of the invention, the process for the storage phase comprises for each sampling capacitor:

application to this sampling capacitor of a voltage equal to the corresponding pixel voltage minus the value of the gate-source voltage of the follower transistor biased with a predetermined constant bias current, for a first predetermined duration so as to obtain for the said sampling capacitor a final state of stable charge,

interruption of the bias current, and

terminating the sampling pulse occurring on completion of a second predetermined duration after the said interruption of the current.

[10] Thus, according to the invention, once the final state of charge has been obtained for each sampling capacitor, the bias current is cut off. Consequently, the gate-source voltage becomes equal to first order to the threshold voltage of the follower transistor. There is consequently less gate-source voltage, thereby making it possible to utilize more useful signal without clipping. Moreover, the white noise contributions due to this bias current disappear with the latter and this consequently results in reduced sampling noise.

[11] More precisely, after interruption of the bias current, the variation in voltage in the bit line is positive and the current required to produce this variation passes through the follower transistor. This current is very weak and the follower transistor is weakly reverse-biased. In this operating zone, the noise band is much reduced and the noise spectral density exhibits a lower amplitude, hence a considerable improvement in the noise.

[12] The second duration is advantageously chosen in such a way as to obtain at the end of each sampling pulse, a residual current flowing through the follower transistor less than a predetermined threshold corresponding to a predetermined threshold level of the noise of the follower transistor.

[13] Thus, by way of indication, the predetermined threshold level for the noise of the follower transistor lies between approximately 50 and 100 microvolts.

[14] Moreover, the first duration is a fraction of the duration of the sampling pulse, the bias current then being greater than a predetermined threshold.

[15] Thus, according to one mode of implementation of the invention, in which the duration of the sampling pulse is of the order of one microsecond, the first duration may be of the order of 100 nanoseconds, and the bias current of the order of 10 microamperes. This makes

it possible, by using a current approximately 10 to 20 times greater than a bias current used in the prior art, to reach stabilization all the more rapidly in respect of the state of charge of each sampling capacitor.

[16] In a general manner, according to the invention, the voltages reached on the sampling capacitors depend only on the two different levels of pixel voltage. The principle is therefore deterministic.

[17] The high current, advantageously used before cut-off, is an element that participates in the obtaining of this deterministic principle.

[18] Likewise, it is advantageous to precharge each sampling capacitor to a predetermined initial value before each sampling pulse. Thus, the precharge makes it possible to begin each sampling from a deterministic state. Specifically, as soon as the current is cut off, the final voltage to which one tends depends on the initial voltage. The precharge makes it possible to lose all "memory" of the voltage sampled in the previous cycle.

[19] The invention also proposes an image sensor, comprising a matrix of active pixels, and means for processing the information delivered by the said matrix of active pixels, the processing means comprising a pair of sampling capacitors per column of the matrix that are able to be respectively linked electrically to the follower transistor tracking each pixel of the column in the course of two respective sampling pulses corresponding respectively to two successive different levels of pixel voltage that are applied to the gate of the follower transistor.

[20] According to a general characteristic of the invention, the processing means comprise a current source connected to each column of the matrix, and able to deliver on

command to the said column a predetermined constant bias current, and control means able for each sampling capacitor and in the course of the corresponding sampling pulse:

energize the column with the said bias current for a first predetermined duration so as to obtain for the said sampling capacitor a final state of stable charge,

then interrupt the energizing of the said column by the bias current, and

end the sampling pulse occurring on completion of a second predetermined duration after the said interruption of the current.

[21] According to one embodiment of the invention, the current source is connected to the said column by an interrupter controllable by the control means.

[22] According to one embodiment of the invention, the processing means comprise precharging means able to precharge each sampling capacitor to a predetermined initial value before each sampling pulse.

[23] More precisely, by way of indication, when each sampling capacitor possesses a terminal linked to ground, the precharging means comprise two additional controllable interrupters able to link respectively the other two terminals of the two sampling capacitors to ground.

[24] This said, it is appropriate to note here that the precharging of the capacitors is not indispensable but makes it possible to gain time to obtain a deterministic state at the end of the first duration. Specifically, with this precharge, since one starts from a deterministic state right from the beginning of the first duration, so will it also be on completion of this first duration.

[25] Likewise, the use of a larger bias current than the customary value also makes it possible to gain time in the obtaining of this deterministic state.

[26] Having regard to the fact that the phenomenon occurring over the second duration is slow, the use in particular of a high bias current, makes it possible to obtain a total duration (first duration + second duration) equivalent to the sample acquisition duration customarily used in the prior art (for example, one microsecond).

[27] However, the advantages of the invention as regards noise reduction in particular, may also be obtained without high value of bias current or precharge, by simply employing a bigger sample acquisition duration.

[28] The invention also proposes an image acquisition device, for example a video camera, comprising at least one image sensor as defined hereinabove.

#### BRIEF DESCRIPTION OF THE DRAWINGS

[29] A more complete understanding of the method and apparatus of the present invention may be acquired by reference to the following Detailed Description when taken in conjunction with the accompanying Drawings wherein:

[30] FIGURE 1 is a schematic of an image sensor according to the invention;

[31] FIGURE 2 illustrates in greater detail a part of the image sensor of FIGURE 1;  
and

[32] FIGURE 3 illustrates a time chart representative of a mode of implementation for the invention.

## DETAILED DESCRIPTION OF THE DRAWINGS

[33] In FIGURE 1, the reference CPT designates an image sensor incorporated for example into a video camera CMV.

[34] The image sensor CPT comprises a pixel matrix PXA organized in rows and columns.

[35] A row decoder RD makes it possible to select the rows of the matrix while a column decoder DCL makes it possible to select the columns BLi (bit line) of the matrix.

[36] Moreover, a pair of sampling capacitors C1, C2 is connected to each column of the matrix by way of sampling transistors, as is illustrated in FIGURE 2.

[37] Finally, reading means MLCT of conventional structure are known per se and allow reading of the charges stored in the sampling capacitor C1, C2. Such reading means may exhibit an architecture allowing voltage-wise reading of the pixel signal, or else an architecture allowing physical transfer of the charges contained in the sampling capacitors into two feedback capacitors connected between the inputs and the outputs of a differential readout amplifier. Such an architecture is for example described in French patent application No. 0300360, the disclosure of which is hereby incorporated by reference. The readout means may also conventionally comprise one analog/digital converter per column.

[38] If reference is now made more particularly to FIGURE 2, it may be seen that each pixel PX comprises a photodiode PD whose cathode is linked to a capacitor (consisting essentially of the diode's own capacitance, that is to say the capacitance of the PN junction of the diode) as well as to the supply voltage by way of a transistor controlled by a reset signal RS.

The cathode of the photodiode PD is also linked to the gate of a follower transistor TS connected to a bit line (column) BL by way of a line selection transistor TSL. This transistor TSL is controlled by a line selection signal SL.

[39] The biasing of the follower transistor TS is effected by bias means PLS connected to the bit line BL. The bias means PLS here comprise a current source and the latter is connected to the bit line BL by way of an interrupter ITS, formed for example of a MOS transistor, controlled by a signal K.

[40] Moreover, at the base of the column BL are connected the two sampling capacitors C1 and C2. In this embodiment, the two terminals B1C1 and B1C2 of the two capacitors C1 and C2 are linked to ground. Moreover, the other terminal B2C1 of the capacitor C1 is linked to the pixel PX by way of a transistor TDS1 controlled on its gate by a control signal CDS1. Likewise, the other terminal B2C2 of the capacitor C2 is linked to the pixel PX by way of a transistor TDS2 controlled on its gate by a control signal CDS2. Moreover, the terminals B2C1 and B2C2 of the two sampling capacitors C1 and C2 may be respectively connected likewise to ground by way of two additional interrupters IT1 and IT2 both controlled by a signal, here dubbed the precharge signal, PRCH.

[41] All the control signals are delivered by control means MCM, embodied for example from voltage sources and logic gates.

[42] The pixel PX is said to be “active” since it contains an amplification device formed in this example by the follower transistor TS. Although only an exemplary active pixel architecture has been represented in FIGURE 2, the luminous signal sensed by the pixel may be in a general manner modeled by a voltage generator applying two different voltage levels  $V_i$

(initial) and  $V_f$  (final) to the gate of the transistor TS in succession. The useful signal  $V_s$  (at the pixel level) thus corresponds to the difference between these two levels  $V_i$  and  $V_f$ .

[43] The transistor TSL is, when it is on, a conducting interrupter, thereby making it possible to connect the source of the follower transistor TS to the bit line. At a given instant, only one pixel is connected thereto, in this instance it is the one belonging to the selected row.

[44] In a conventional manner known per se, the bias current provided by the source PLS biases, current-wise, the follower transistor TS of the pixel of the selected row. This transistor TS is therefore biased as a follower. Consequently, the potential of its source reproduces that of its gate, to within an offset  $V_{gs}$ . Stated otherwise, the signal voltage  $V_s$  is reproduced on the bit line, to within an offset  $V_{gs}$ . The voltage VBL on the bit line BL is therefore equal to  $V_s - V_{gs}$ .

[45] Moreover, when the signal  $V_s$  provides the level  $V_i$ , a first sample is tapped off from the sampling capacitor C1 by actuating the transistor TDS1 through the command CDS1. This command CDS1 is a pulse that remains active for a microsecond for example.

[46] When the signal  $V_s$  provides the level  $V_f$ , a second sample is tapped off from the sampling capacitor C2 by actuating the transistor TDS2 through the command CDS2. This command CDS2 is likewise a sampling pulse that remains active likewise for approximately one microsecond. Eventually, the useful signal is available at the instants of deactivation of signals CDS1 and CDS2 in the form of the differential voltage  $\Delta V$  present between the two sampling capacitors C1 and C2. Also, it is this differential voltage that will for example be amplified in the readout means MLCT.

[47] Relative to a conventional manner of operation of this type, the manner of operation of the invention will now be described while referring more particularly to FIGURE 3, in which the sampling pulses CDS1 and CDS2 have in particular been reproduced. The duration T of each sampling pulse has been held at one microsecond.

[48] It may be seen in particular in this FIGURE 3 that the bias current IPOL, delivered by the current source PLS, is provided only for a small fraction T1 of the duration of each sampling pulse CDS1, CDS2. This current IPOL is thereafter cut off by means of the interrupter ITS controlled by the control signal K.

[49] This first duration T1 is predetermined so as to obtain for the sampling capacitor concerned, a stable final state of charge. In the preferred mode of implementation that is described here, the nominal value of the bias current  $I_{POL}$  is much greater than that used in conventional architectures, typically of the order of 10 to 20 times larger. This allows the level of the voltage  $V_{BL}$  to be stabilized all the more rapidly. By way of example, for a sampling pulse of the order of one microsecond, the first duration T1 is for example of the order of 100 nanoseconds with a bias current of the order of 10 microamperes.

[50] On completion of the duration T1 there is a stable final state of charge in the sampling capacitor concerned, that is to say a zero current through this sampling capacitor, to within a tolerance.

[51] When the bias current  $I_{POL}$  is cut off, a very rapid decay of the current then occurs over the second duration T2 equal to T-T1. The gate-source voltage of the follower transistor then goes from

$$V_t + \sqrt{\frac{I_{POL}}{K}}$$

to the threshold voltage  $V_t$ ,  $K$  being a technological constant.

[52] There is therefore less gate-source voltage, thereby making it possible to utilize more useful signal without clipping.

[53] Moreover, the white noise contributions due to the bias current (follower transistor and current source) disappear with the latter, hence resulting in reduced sampling noise.

[54] More precisely, when the current is cut off, the potential  $V_{BL}$  of the bit line BL goes, depending on the value  $V_i$  or  $V_f$  of the pixel voltage, from

$$V_{i,f} - V_t - \sqrt{\frac{I_{POL}}{K}}$$

to  $V_{i,f} - V_t$ .

[55] The voltage variation is positive and the current required to produce this variation passes through the follower transistor. This current rapidly attains a very low value (typically less than 100 nanoamperes), and the follower transistor is weakly reverse-biased. In this operating zone, the noise band is much reduced and the noise spectral density exhibits a low amplitude, hence a considerable improvement in the noise.

[56] It is also particularly advantageous, although not indispensable, to impart a deterministic state to each sampling capacitor before each sampling. A solution then consists, as illustrated in FIGURE 3, in precharging the sampling capacitors C1 and C2 to a zero voltage before each sampling pulse.

[57] Although preferred embodiments of the method and apparatus of the present invention have been illustrated in the accompanying Drawings and described in the foregoing Detailed Description, it will be understood that the invention is not limited to the embodiments disclosed, but is capable of numerous rearrangements, modifications and substitutions without departing from the spirit of the invention as set forth and defined by the following claims.